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Ø Û (Microsoft QuickBasic version 1.1)

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Modeling Deficit Irrigation Water Requirement For Maize in Mosul Region

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Abstract

A computerized model with (Microsoft QuickBasic version 1.1) was proposed for simulating the effect of deficit irrigation for maize crop during spring and autumn seasons in Mosul region. The simulation is based on 16 years of climatological data for the period (1985-2000) for Mosul meteorological station , which includes daily maximum and minimum temperatures , maximum and minimum relative humidity , wind speed at 2m height , and sunshine hours , which is used to calculate daily reference evapotranspiration with Penman-Monteith equation .The model predicts yield reduction by changing irrigation depth for three different irrigation methods (sprinkler , furrow and drip) .The rainfall is divided into three classes which represent three regions (wet ,semi- arid and arid).

$$\frac{ET_c}{ET_{c_{adj}}} = \frac{K_c}{K_{cb}}$$

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$$ETc_{adj} = (Ks * Kcb + Ke)ETo \text{-----}(1)$$

: \hat{a}
 (/) \hat{U} () - : ETc_{adj}
 \hat{U} : Ks
 . (\hat{U}) \hat{U} \hat{U} : Kcb
 . () \hat{U} : Ke
 \hat{U} \hat{U} Ks \hat{U}
 \hat{O} (Kcb) \hat{O} \hat{U} \hat{U} . \hat{U} ,
 \hat{O} ETo - ETc \hat{U} -
 Kcb \hat{U} . \hat{U}
 \hat{O} . (0-1.4) \hat{O} Kcb , \hat{U} \hat{U} Kc
 \hat{O} \hat{U} Kcb \hat{U} \hat{U}
 \hat{O} \hat{O} \hat{U} (2)
 \hat{O} \hat{O} \hat{O} \hat{U} \hat{O} , \hat{O} \hat{O} \hat{U} \hat{O} \hat{O} \hat{O} \hat{O}
 : (FAO,1998) \hat{U} \hat{U} \hat{U} (2)

$$Kcb_i = Kcb_{prev} + \left[\frac{i - \sum(L_{prev})}{L_{stage}} \right] [Kcb_{next} - Kcb_{prev}] \text{-----}(2)$$

: \hat{a}
 \hat{U} : i
 i \hat{U} \hat{U} : Kcb_i
 \hat{U} \hat{U} : Kcb_{prev}
 () \hat{U} : L_{stage}
 () \hat{U} \hat{U} : $\sum(L_{prev})$
 \hat{O} , \hat{U} (1) \hat{U} Kcb
 .% 45 (/)2

.(FAO, 1998) \hat{O} (Kcb) \hat{O} \hat{O} (1) \hat{O}

0.15	1.15	←	0.15	



(2)

\bar{O} \bar{O} \bar{O} (Kcb) \bar{U} \bar{U}

: (FAO,1998)

$$K_{cb} = K_{cb} \text{ (جدول 1)} + [0.04 (U^2 - 2) - 0.004 (RH_{min} - 45)] \left(\frac{h}{3}\right)^{0.3} \text{-----(3)}$$

: \hat{a}

\bar{O} \bar{O} \bar{O} \bar{O} \bar{U} \bar{O} 2 \bar{O} \bar{O} \bar{O} \bar{O} \bar{U} \bar{O} : U^2
(/)

(%) \bar{U} \bar{U} : RH_{min}

\bar{O} \bar{O} \bar{O} \bar{O} \bar{U} \bar{O} \bar{U} \bar{O} \bar{O} \bar{O} : h
()

\bar{O} \bar{O} (Ke) \bar{U}

:(FAO,1998) (Ze)

$$K_e = \min(K_r(K_{c_{max}} - K_{cb}), f_{ew} * K_{c_{max}}) \text{-----(4)}$$

: \hat{a}

\bar{U} \bar{U} : K_r

K_c \bar{O} : $K_{c_{max}}$

: f_{ew}

\bar{O} \bar{U} , -
- \bar{O} \bar{O} \bar{O} . , \bar{U}
 \bar{U} \bar{O} \bar{O} - \bar{O} \bar{O} \bar{O} \bar{U} \bar{O} \bar{O} \bar{O}
(Sumner,1996)

\bar{O} \bar{O} \bar{O} \bar{O} \bar{O} \bar{O} 16 \bar{U} \bar{O} \bar{O} \bar{O} \bar{O}
, \bar{O} \bar{O} \bar{U} \bar{U} (2000 – 1985)
- 2 , -

$$ET_o = \frac{0.408\Delta(R_n - G) + \gamma \frac{900}{(T + 273)} U^2 (e_s - e_a)}{\Delta + \gamma(1 + 0.34U^2)} \text{-----(5)}$$

: \hat{a}

(/) - : ET_o

(/ \bar{U}) \bar{U} : Δ

(.² / \bar{U}) : R_n

$$\begin{aligned}
 & \left(\frac{U_2}{U} \right) : G \\
 & \left(\frac{U}{U} \right) : \gamma \\
 & \left(\frac{U}{U} \right) : T \\
 & \left(\frac{U}{U} \right)^2 : U2 \\
 & \left(\frac{U}{U} \right) : es \\
 & \left(\frac{U}{U} \right) : ea \\
 & \left(\frac{U}{U} \right) : (es - ea) \\
 & \text{FAO, 1998}
 \end{aligned}$$

$\left(1 - \frac{y_a}{y_m} \right) = K_y \left(1 - \frac{ETc_{adj}}{ETc} \right)$ (FAO, 1998)

$$\left(1 - \frac{y_a}{y_m} \right) = K_y \left(1 - \frac{ETc_{adj}}{ETc} \right) \text{-----(6)}$$

$\left(\frac{U}{U} \right) : y_a$
 $\left(\frac{U}{U} \right) : y_m$
 $\left(\frac{U}{U} \right) : ETc_{adj}$
 $\left(\frac{U}{U} \right) : ETc$
 $\left(\frac{U}{U} \right) : K_y$

$\left(1 - \frac{ETc_{adj}}{ETc} \right) - (1 - y_a / y_m)$
 Cavero et al (2000) (Soil Water Stress) (Simulation models)

(15%) (30%)

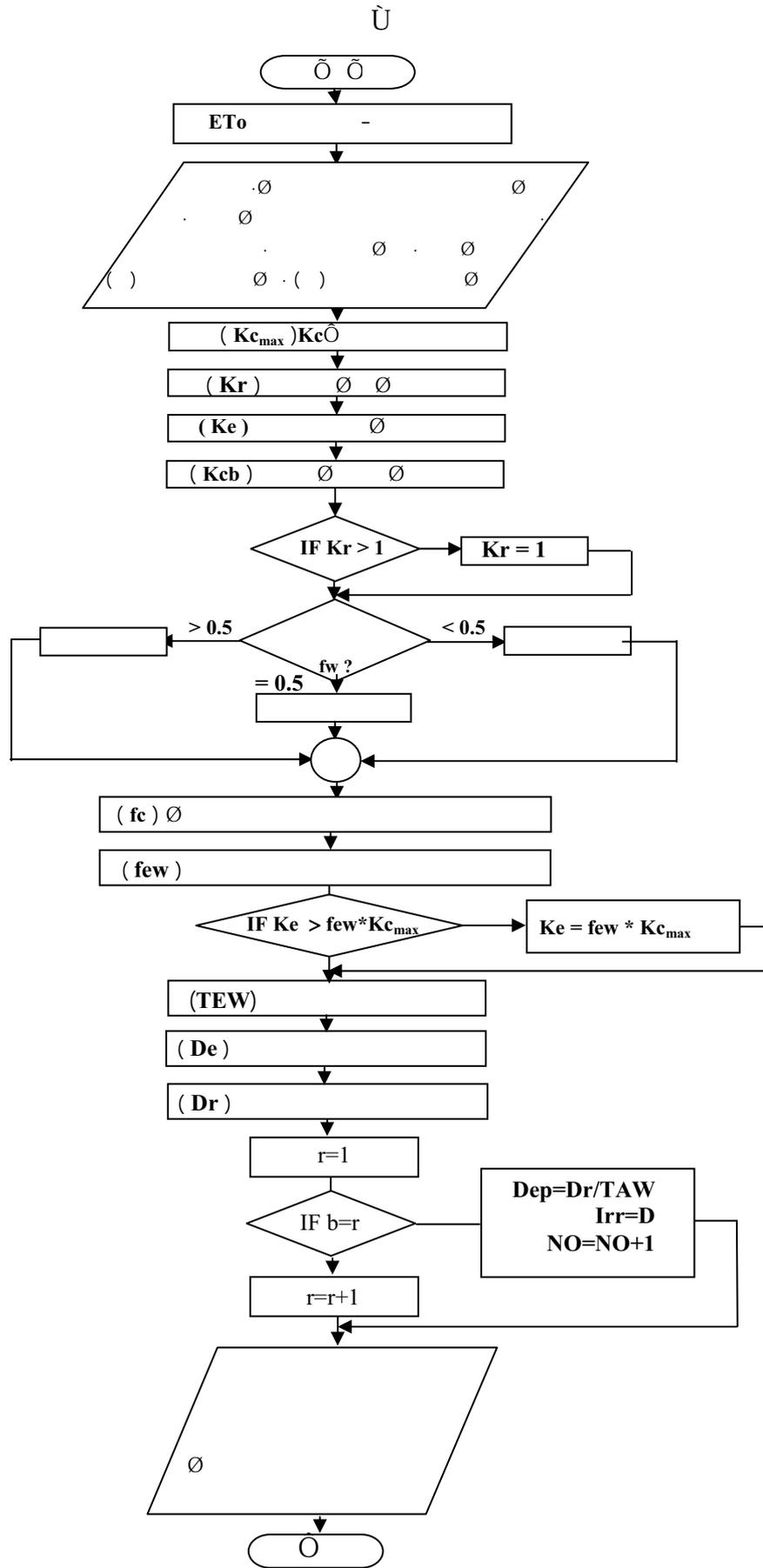
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 (Microsoft QuickBasic version 1.1)
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 :LOS (Õ) :NDI $\left[\frac{(NDI - LOS)}{NDI} \right] * 100$
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()	()	()	()	() (FAO,1992)	
30	30	20	10	10 - 30	
60	60	45	30	30 - 60	
80	80	55	30	30 - 80	

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(%)	(IWR)	(CU) ()	(NDI) ()	
17	446	495	170	
2	536	608	510	
2	540	618	510	

() (4)Ø

(%)	(IWR)	(CU) ()	(NDI) ()	
31	560	480	340	
.6	597	648	765	
.2	611	670	935	

() (5)Ø

(%)	(IWR)	(CU) ()	(NDI) ()	
15	605	542	510	
0	634	661	1020	
0	634	661	1360	

(6)Ø

(%)	(IWR)	(CU) ()	(NDI) ()	
23	645	522	480	
3.7	671	667	960	
2.5	679	675	1280	

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